



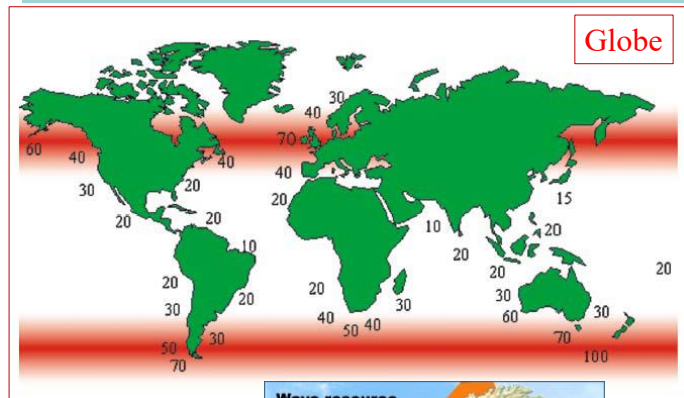
Challenges and Progress in Wave Energy Technologies

Dr. Wanan Sheng

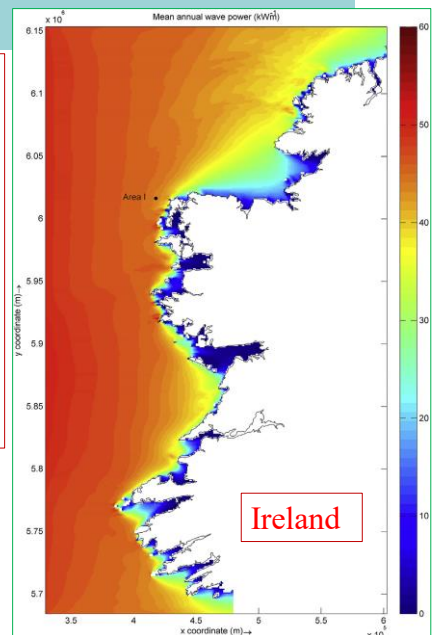
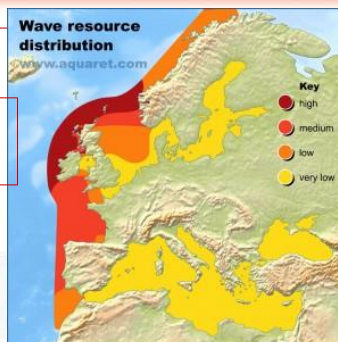
MaREI Centre, ERI, University College Cork, Ireland



Wave energy Resources



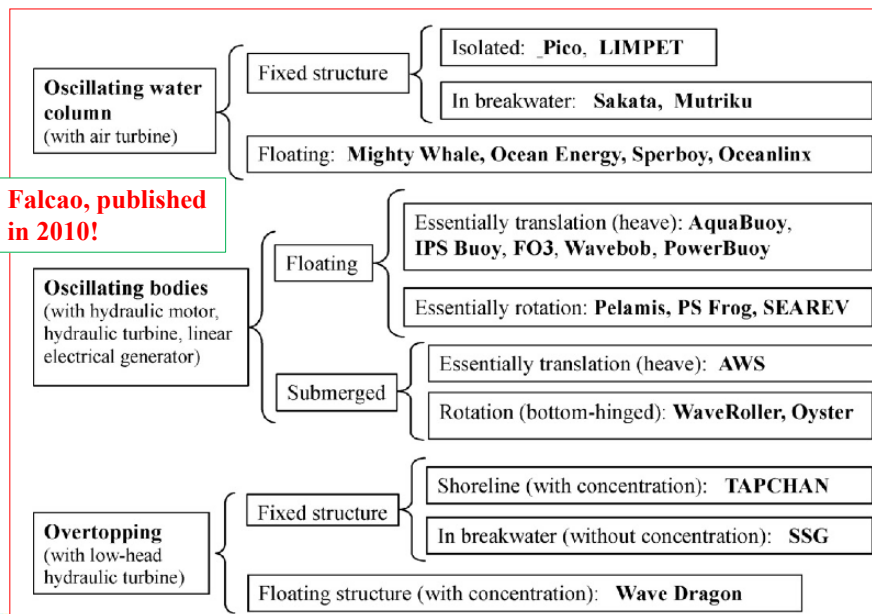
**Atlantic
Arc**



- $\sim 70 \text{ kW/m}$ annually
- 100km=demand of electricity in Ireland



Wave energy converters: technology convergence?



Falcao, published in 2010!

▪ Efficiency?

▪ Initial cost?

▪ Reliability?

Q: when will we see a 50MW wave farm? (ICOE 2012)

• For optimists (very soon?)

- Pre-commercial full-scale grid connection or sea trials: Pelamis, Oyster, OWC plants...
- MEA (**Carbon Trust-Marine Energy Accelerator**) baseline costs for current technologies, **Wave: 38-48p/kWh, Tidal: 29-33p/kWh (JRC report 2014: €0.70-1.05/kWh for Wave; €0.50-0.65/kWh for Tidal).**
- MEA cost reduction strategies: 18-20p/kWh, i.e. ~ 39% reduction for tidal devices.
- Cost reduction through technology innovations/massive production...

• For pessimists

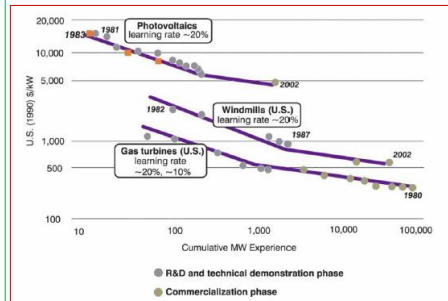
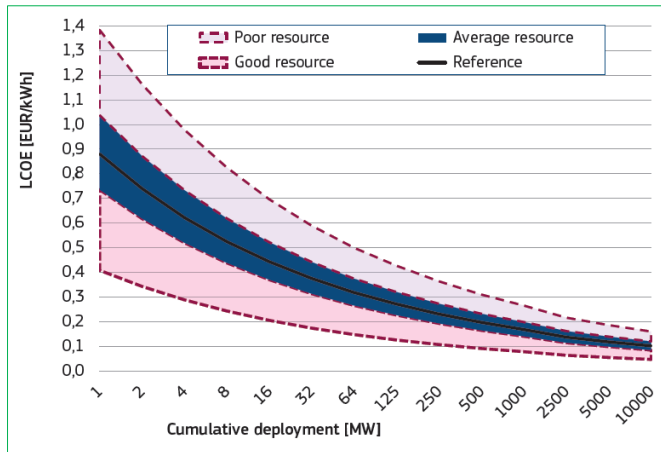
- A fear that all technologies may fail: too many failures and too few successes so far.
- Real cost of wave energy still unknown for most developers and researchers.
- Lack of assessment methods and standardizations.
- Too many technical and non-technical barriers.
- Theory development limited...

Pathways to reduce the cost of ocean energy

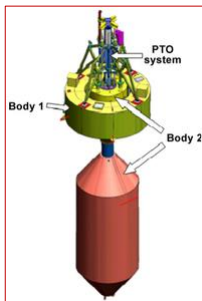
➤ Targets (OEE 2016) on ocean energy costs:

- Tidal LCoE could reach €10/kWh by 2030
- Wave LCoE could reach €10/kWh by 2035

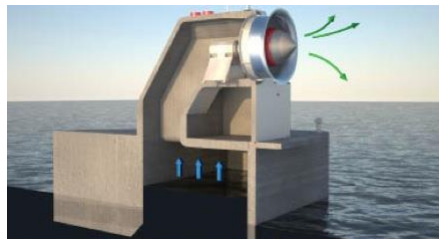
- Large scale/volume production
- Experience (learning curves)
- Technology innovations



Reality: Failures



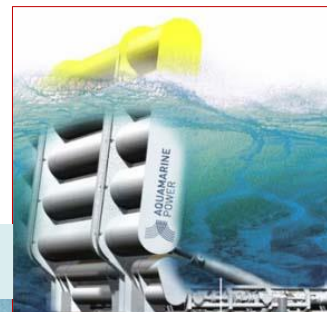
WaveBob (Ireland)
Bankrupt in 2013



Oceanlinx OWC (Australia)
Company bankrupt in 2010
Bought by a Taiwanese company

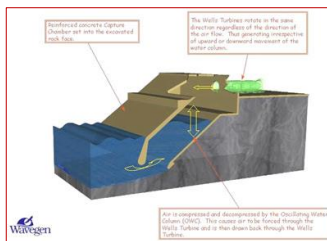


Pelamis (Scotland)
Bankrupt in 2014

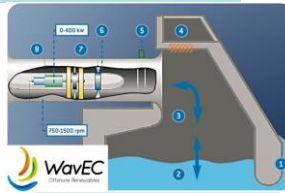


Oyster (Scotland)
Bankrupt in 2015

Reality: Successes (?)



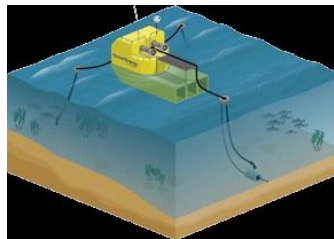
Scotland
LIMPET OWC plant in operation since 2000, generated power >60,000hrs in 10 years
Now in decommissioning



Portugal
PICO OWC plant, still operational



Spain
Mutriku OWC plant, still operational



Ireland
OE Buoy OWC device, 1/4 scale sea trials in Galway Bay >3 years
Full commercial device in construction (will be a sea trial for one year in Hawaii in 2018).



Technical challenges in wave energy conversions

Power conversion equation:

$$P = F \cdot V$$

To generate a large power:

- with a very high speed in conventional power generation (e.g., steam turbines): **high reliability and high energy conversion efficiency**
- with a very large force (because of the small speed) for wind, tidal and wave energy: **low reliability and low energy conversion efficiency**

For wave energy (wave period: 6-11s):

- Large force and low speed for wave energy conversion (also with reciprocating motion/velocity and force):
 - **fatigue problems: reliability problem**
 - **low conversion efficiency: high energy cost**

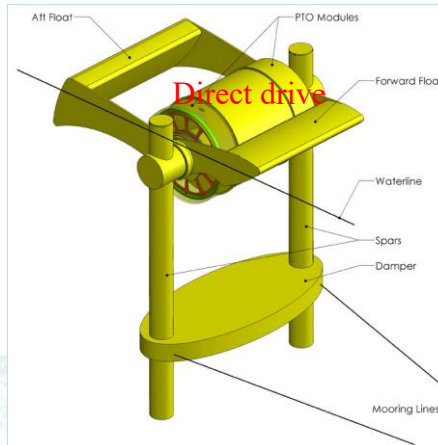


PTO reliability



PTO (power take-off)

- Hydraulics/Ram
- Direct drive
- Air/water turbine

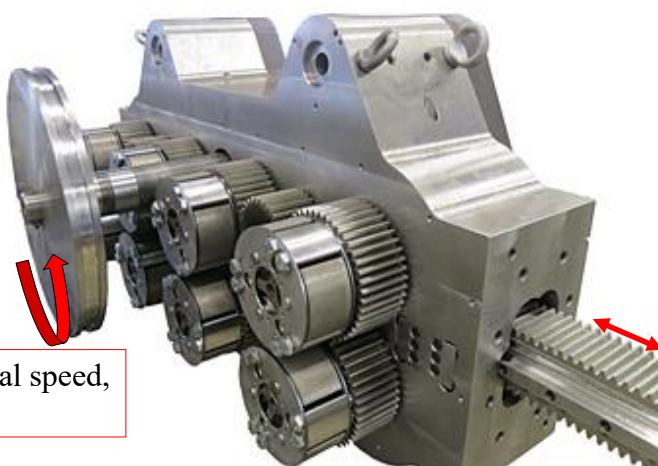


Blue power
energy PTO

PTO reliability: specialized gear box

to generator

High rotational speed,
low torque



to WEC

Large force
Low speed

Dynamic systems: wave energy conversion

Newton's 2nd Law:

$$m\ddot{\mathbf{x}} = \mathbf{F}_{total}$$

Generic dynamic equation for wave energy devices, with PTO, control and mooring systems:

$$[\mathbf{M} + \mathbf{A}(\infty)] \cdot \ddot{\mathbf{x}}(t) + \int_{-\infty}^t \mathbf{B}(t - \tau) \cdot \dot{\mathbf{x}}(\tau) d\tau + \mathbf{C} \cdot \mathbf{x}(t) = \mathbf{X}(t) + \mathbf{F}_{PTO} + \mathbf{F}_{mooring} + \mathbf{F}_{control}$$

Power extraction: $P(t) = \mathbf{F}'_{PTO}(t) \cdot \dot{\mathbf{x}}(t)$

Big question: how can we calculate or model these forces (each term) so that we can optimise the device or improve wave energy conversion efficiency?

- Physical modelling
- Numerical simulation



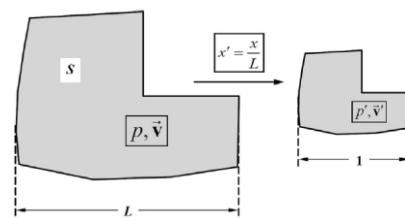
Physical modelling (1): Why and How

$$[\mathbf{M} + \mathbf{A}(\infty)] \cdot \ddot{\mathbf{x}}(t) + \int_{-\infty}^t \mathbf{B}(t - \tau) \cdot \dot{\mathbf{x}}(\tau) d\tau + \mathbf{C} \cdot \mathbf{x}(t) = \mathbf{X}(t) + \mathbf{F}_{PTO} + \mathbf{F}_{mooring} + \mathbf{F}_{control}$$

Fundamental requirements:

(1) **Meaningful:** geometrical similarity must be satisfied.

(2) **Useful:** kinematic and dynamic similarities must be **partially or fully** satisfied. For instance, the data from a scale model are used to predict the prototype/full scale.



$$\begin{cases} \frac{\partial u'}{\partial t'} + u' \frac{\partial u'}{\partial x'} + v' \frac{\partial u'}{\partial y'} + w' \frac{\partial u'}{\partial z'} = -\frac{1}{2} \frac{\partial p'}{\partial x'} + \frac{1}{Re} \left(\frac{\partial^2 u'}{\partial x'^2} + \frac{\partial^2 u'}{\partial y'^2} + \frac{\partial^2 u'}{\partial z'^2} \right) \\ \frac{\partial v'}{\partial t'} + u' \frac{\partial v'}{\partial x'} + v' \frac{\partial v'}{\partial y'} + w' \frac{\partial v'}{\partial z'} = -\frac{1}{2} \frac{\partial p'}{\partial y'} + \frac{1}{Re} \left(\frac{\partial^2 v'}{\partial x'^2} + \frac{\partial^2 v'}{\partial y'^2} + \frac{\partial^2 v'}{\partial z'^2} \right) \\ \frac{\partial w'}{\partial t'} + u' \frac{\partial w'}{\partial x'} + v' \frac{\partial w'}{\partial y'} + w' \frac{\partial w'}{\partial z'} = -\frac{1}{2} \frac{\partial p'}{\partial z'} - \frac{1}{Fr^2} + \frac{1}{Re} \left(\frac{\partial^2 w'}{\partial x'^2} + \frac{\partial^2 w'}{\partial y'^2} + \frac{\partial^2 w'}{\partial z'^2} \right) \end{cases}$$

$$Re = \frac{\rho LU}{\mu} > 10^5$$

Sheng, W., Alcorn, R., Lewis, T., "Physical modelling of wav energy converters," *Ocean Engineering*, Vol. 84, (2014), pp.29-36.



Physical modelling (2): Pros and Cons

Advantages:

- Full physical phenomena if modelling is appropriate.
- Controlled lab conditions to isolate dynamic effects (e.g. regular waves).
- Easy and accurate measurements.
- Fast optimisation process
- Installation and removal of device
- Cost: cheap, when compared to full scale sea trials .

Disadvantages:

- Scaling effects: **how large the model is appropriate?**
- Power take-off (PTO)/control system: **is correctly modelled?**
Feasibility problem!
- Energy conversion system: **can we do this? (~1W in model scale)**
- Cost: expensive, when compared to numerical modelling.

Dynamic systems: numerical simulation

Solution to the time domain equation

$$[M + A(\infty)] \cdot \ddot{x}(t) + \left(\int_{-\infty}^t B(t-\tau) \cdot \dot{x}(\tau) d\tau \right) + C \cdot x(t) = x(t) + F_{PTO} + F_{mooring} + F_{control}$$

Diagram illustrating the time domain equation for dynamic systems, with annotations:

- W=WAMIT** (above the equation)
- W** (below $[M + A(\infty)]$)
- W** (below $\int_{-\infty}^t B(t-\tau) \cdot \dot{x}(\tau) d\tau$)
- ?** (below $\dot{x}(\tau)$)
- W** (below $C \cdot x(t)$)
- ?** (below $x(t)$)
- ?** (below F_{PTO})
- ?** (below $F_{control}$)

Device assessment and optimisation using WAMIT

How to optimise PTO and control the device for improving wave energy production?

How to solve the convolution term in the time-domain equation?

Solution 1: Convolution calculation

Time domain equation

$$[\mathbf{M} + \mathbf{A}(\infty)]\ddot{\mathbf{x}}(t) + \int_{-\infty}^t \mathbf{K}(t-\tau)\dot{\mathbf{x}}(\tau)d\tau + \mathbf{C} \cdot \mathbf{x}(t) = \mathbf{X}(t) + \mathbf{F}_{PTO} + \mathbf{F}_{mooring} + \mathbf{F}_{control}$$

Step 1:

$$K(t) \approx \sum_{k=1}^N \alpha_k e^{\beta_k t}$$

The Prony approximation to impulse function

Step 2:

$$I(t) = \int_0^t K(t-\tau)\dot{\zeta}(\tau)d\tau$$

$$I(t) = \sum_{k=1}^N I_k(t)$$

with

$$I_k(t) = \alpha_k e^{\beta_k t} \int_0^t e^{-\beta_k \tau} \dot{\zeta}(\tau) d\tau$$

Step 3:

$$I_k(n+1) = I_k(n)e^{\beta_k \Delta t} + \dot{\zeta}(n)\Delta t \alpha_k e^{\beta_k \Delta t/2}$$

Recursive!

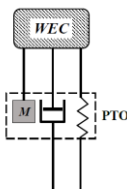
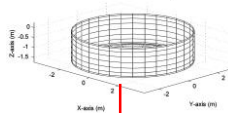
W. Sheng, R. Alcorn, A. Lewis, 'A new method for radiation forces for floating platforms in waves', *Ocean Engineering*, 105(2014)43–53



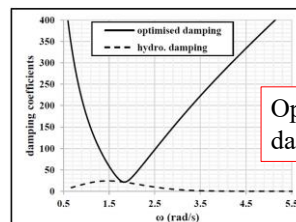
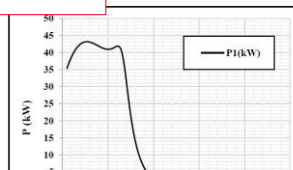
Solution 2: PTO Damping and device optimization (in regular waves)

$$[\mathbf{M} + \mathbf{A}(\infty)]\ddot{\mathbf{x}}(t) + \int_{-\infty}^t \mathbf{K}(t-\tau)\dot{\mathbf{x}}(\tau)d\tau + \mathbf{C} \cdot \mathbf{x}(t) = \mathbf{X}(t) + \mathbf{F}_{PTO} + \mathbf{F}_{mooring} + \mathbf{F}_{control}$$

- A point absorber: $D=6\text{m}$, draft= 1.5m
- PTO optimal damping in regular waves

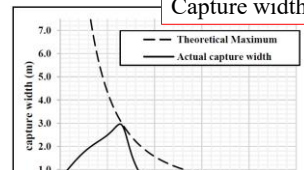


Maximal power
($H=2\text{m}$)



Optimised PTO damping

Capture width



Sheng, W., R. Lewis, T., 'Power take-off optimisation for maximising energy conversion of wave activated bodies', *IEEE Journal of Oceanic Engineering*, 2015. DOI: 10.1109/JOE.2015.2489798.

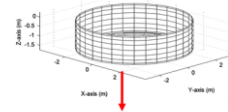
Solution 3: Control (latching control)

$$[\mathbf{M} + \mathbf{A}(\infty)]\ddot{\mathbf{x}}(t) + \int_{-\infty}^t K(t-\tau)\dot{\mathbf{x}}(\tau)d\tau + \mathbf{C} \cdot \mathbf{x}(t) = \mathbf{X}(t) + \mathbf{F}_{PTO} + \mathbf{F}_{mooring} + \mathbf{F}_{control}$$

Fundamental challenges in active control:

- (1) Physical implementation: how to make the control.
- (2) Time horizon into future (~10-20s).

A point absorber: $D=6\text{m}$, draft= 1.5m

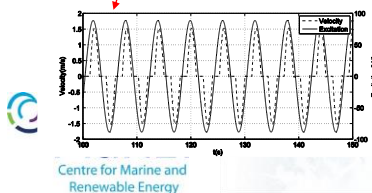
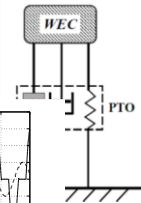
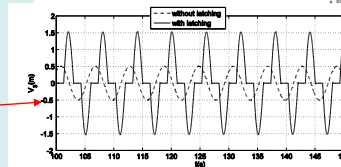


Latching for phase control

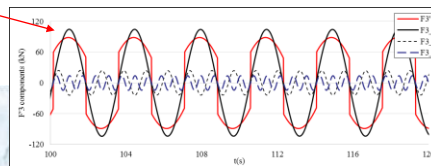
- Latching when velocity is zero or very small, for instance, use a clamp or breaking system.
- Latching duration T_{latch}

Improvement of wave energy conversion in terms of

- Phase control
- Motion acceleration
- Excitation increase



Centre for Marine and Renewable Energy

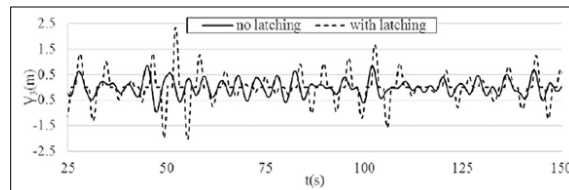
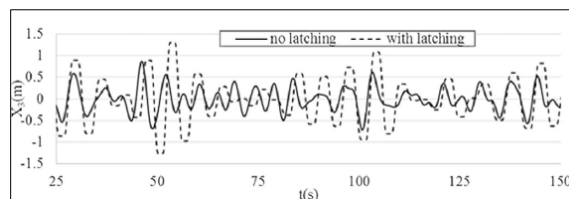


Solution 3: novel latching control

$$T_{latch} = \frac{T_e - T_0}{2}$$

($H_s=1.0\text{m}$, $T_e=6.0\text{s}$)

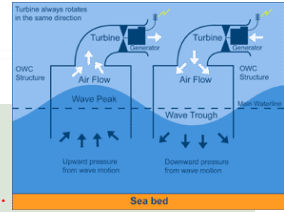
Power conversion increase by 320%!
($H_s=1.0\text{m}$, $T_e=6.0\text{s}$)



1. **Sheng, W.**, Alcorn, R., Lewis, T., "On improving wave energy conversion, Part I: optimal and control technologies", *Renewable Energy* **75** (2015), pp. 922-934. doi:10.1016/j.renene.2014.09.048.
2. **Sheng, W.**, Alcorn, R., Lewis, T., "On improving wave energy conversion, Part II: development of latching control technologies", *Renewable Energy* **75** (2015), pp. 935-944. doi:10.1016/j.renene.2014.09.049.

Why Oscillating Water Column (OWC)?

- **A very adaptive and well-proven concept**
 - Shoreline, nearshore or offshore: bottom-fixed and floating.
 - LIMPET plant: > 60,000 hours in 10 years; OE Buoy sea-trial > 3 years.
- **Structural reliability**
 - **No moving components**
 - **no joints/articulations, thus no significant stress concentration**
 - **no end-stop problem!**
- **High reliability for power take-off**
 - Small force for a certain power take-off due to high speed air flow and rotational speed.
 - Small size generator, probably off-the-shelf !
- **High primary/secondary wave energy conversion efficiency**
 - Novel turbines with very high energy conversion efficiency (~90%).
 - Novel OWC for good power performance.
- **Fewer engineering problems**
 - Power conversion is through a high speed air flow.
 - High speed rotary PTO machine for direct connection to generator and for reducing size of PTO.
 - No significant sealing and wearing issues.



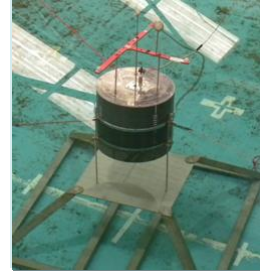
Understanding OWC wave energy converters

- **Hydrodynamics of OWCs**
 - Interaction of OWC and waves.
 - Internal water surface motions (or pressure distribution on IWS).
- **Air flow and compressibility (thermodynamics)**
 - “Spring effect” in full scale air chamber.
 - Difficulties in model test, hence a reliable numerical analysis is needed.
- **Time-domain analysis**
 - Numerical tool for primary wave energy conversion
 - Detailed validations using experimental data
 - Air compressibility included

Time-Domain analysis: hydrodynamics and thermodynamics

$$[M_{99} + A_{99}(\infty)]\ddot{x}_9 + C_{99}x_9 + b_{99}\dot{x}_9 + \int_0^t K_{99}(t-\tau)\dot{x}_9(\tau)d\tau = F_9 - A_0 p$$

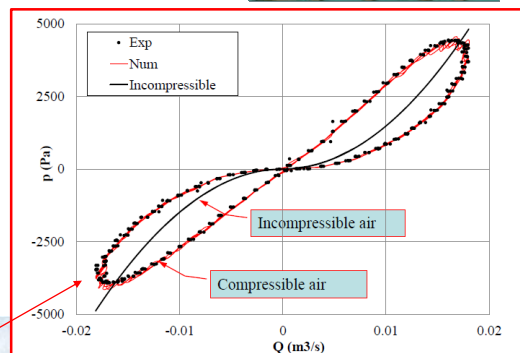
Chamber pressure



$$\frac{dV}{dt} + \frac{V}{\gamma p_0 + p} \frac{dp}{dt} + \frac{-k_1 + \sqrt{k_1^2 + 4k_2 p}}{2k_2} = 0$$

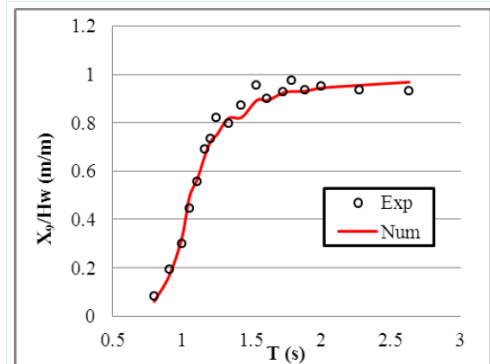
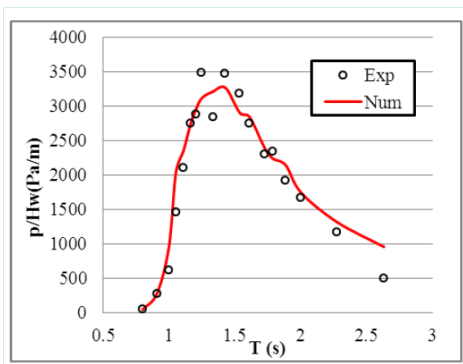
$$\left(1 + \frac{p}{\gamma p_0}\right) \frac{dV}{dt} + \frac{V}{\gamma p_0} \frac{dp}{dt} + \frac{k_1 - \sqrt{k_1^2 - 4k_2 p}}{2k_2} = 0$$

$$V = V_0 - A_0 x_9$$



Sheng, W., Alcorn, R. Lewis, T., "On Thermodynamics of OWC Wave Energy Converters," *Journal of Renewable and Sustainable Energy* 5, 023105 (2013); doi: 10.1063/1.4794750

Comparison: OWC model



1. Sheng, W., Alcorn, R., Lewis, T., "Assessment of primary energy conversions of oscillating water columns. I. hydrodynamic analysis," *Journal of Renewable and Sustainable Energy* 6, 053113 (2014); doi: 10.1063/1.4896850.
2. Sheng, W., Alcorn, R., Lewis, T., "Assessment of primary energy conversions of oscillating water columns. II. power take-off and validations," *Journal of Renewable and Sustainable Energy* 6, 053114 (2014); doi: 10.1063/1.4896851.

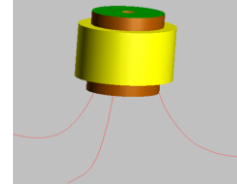


OWC: novel development

IDF application: Efficient shallow water OWC wave energy converter
(IDF No. IDF 13-08)

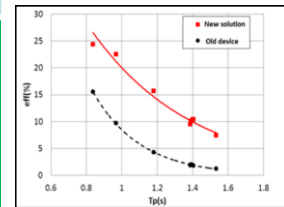
Advantages: shallow water OWC

- Fabricated and fully assembled in harbour/shipyards.
- Concrete structure for low cost and high reliability
- Towed to deployment site and a 'plug-in' type installation requiring a small weather window.



Problems addressed:

- **Significant increase in wave energy conversion efficiency**
- **Much improved performance of the device**
 - ✓ Beneficial for mooring and cable connections.
 - ✓ Beneficial to the accessibility for O&M.



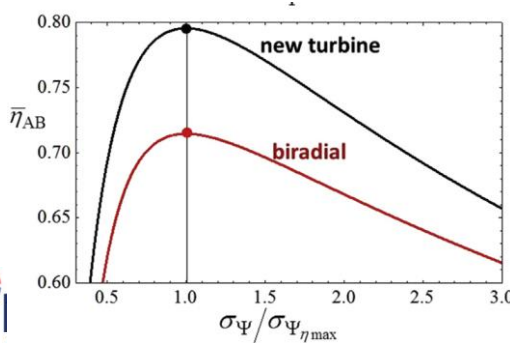
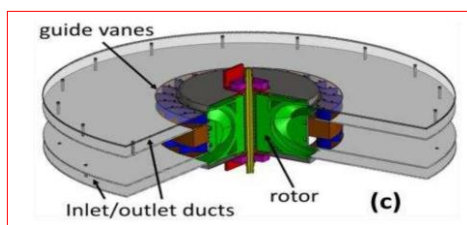
What next?



- 1) contribution to MaREI fundamental research.
- 2) a novel device used for H2020 LCE proposal (2017), scored 8.5/10, missed the cut @9/10 (03/2017)...
- 3) Seeking funds for advancing the technology

New air turbines for OWC devices

Bi-radial turbine



Twin-rotor turbine

